

U.S. Department of Energy

HelioCon

Heliostat Consortium for
Concentrating Solar-Thermal Power

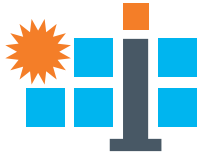
Wind Tunnel Study on the Effects of Ground Clearance Ratio on Heliostat Dynamic Wind Loads

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16 July 2024 • ASME ES2024 • Anaheim

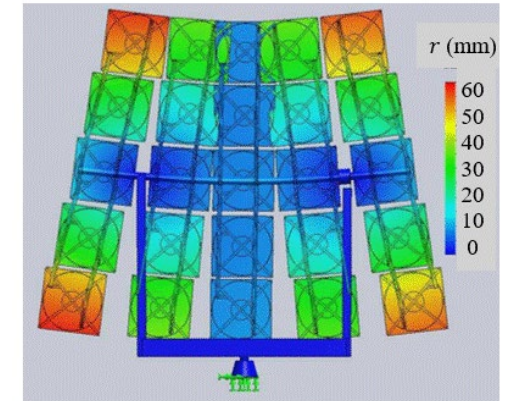
conceptual design • components • integration • mass production • heliostat field

Introduction

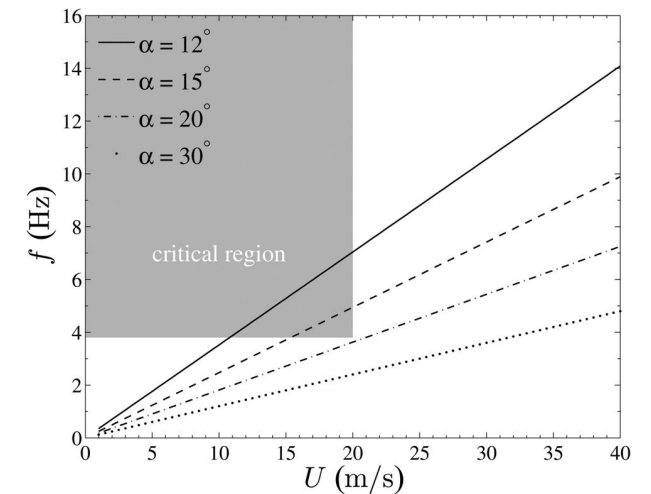


- Dynamic wind loads on operating heliostats
 - Torque bending at modal frequency of 3 Hz corresponds to maximum displacements of 60mm of corner facets (Griffith *et al.* 2015)
 - Out-of-plane torsion and rigid body modes of the mirror frame due to oscillation about the elevation axis cause deflections of the order of 1% of the heliostat characteristic length (Vásquez-Arango *et al.* 2015)
 - Truss member to torque tube interfaces due to out-of-plane bending modes due to wind cause maximum beam deviations of 0.17m and 1.58m, compared with 0.1m and 0.25m due to gravity in the absence of wind (Ho *et al.* 2012)
 - Modal frequencies largely dependent on heliostat size (Ho *et al.* 2012)
- Vortex-induced vibrations induced by wind load fluctuations on a heliostat “flat plate” model depend on elevation angle α , flat plate geometry c and inflow conditions

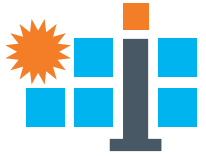
$$St = fc/U$$



NSTTF heliostat FEA simulation
(adapted from Griffith *et al.* 2015)

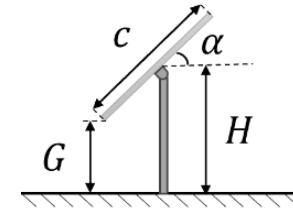


Vortex shedding frequencies (Vásquez-Arango *et al.* 2015)

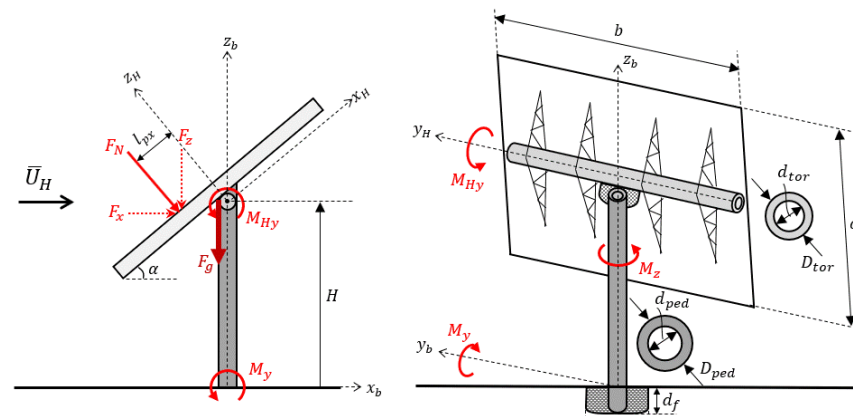


Objectives

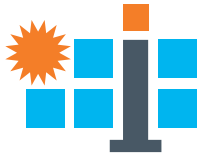
- Investigate the sensitivity of Strouhal number of a single heliostat to:
 - Elevation angle α
 - Ground clearance ratio $GR = G/H$
 - Inflow turbulence



- Spectral analysis of wind load fluctuations measured on a single heliostat using a six-axis load cell and differential pressure sensors

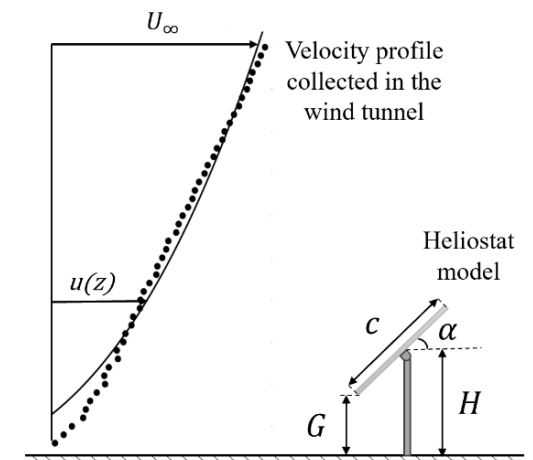
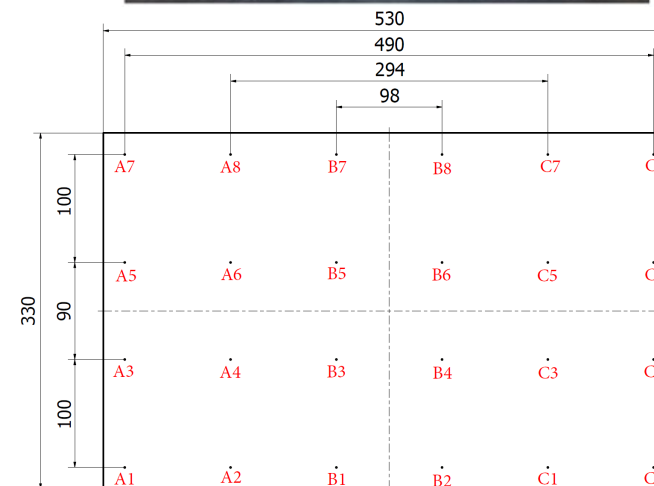
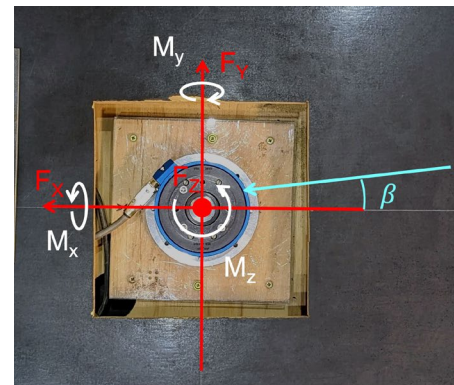
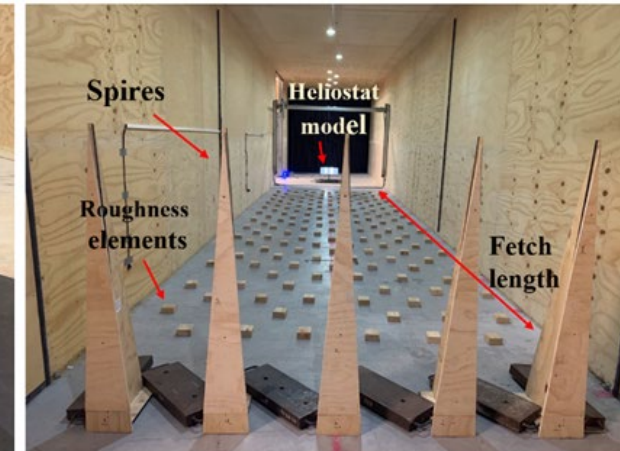
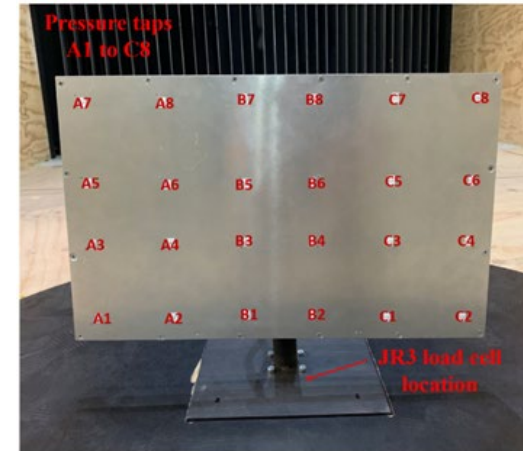


Wind loads on a heliostat (Emes *et al.* 2020)



Wind tunnel experiments – instrumentation

- Two inflow conditions: (1) uniform flow (2) turbulent ABL
- 1:6 scale heliostat model
 - $b = 0.33$ m, $c = 0.53$ m, $H = 0.2$ - 0.325 m
- JR3 six-axis load cell ($G/H = 0.106$ - 0.485)
 ± 100 N F_x, F_y , ± 200 N F_z , ± 12 Nm M_x, M_y, M_z with $\pm 0.25\%$ accuracy
- 24 differential pressure sensors
 $\pm 1''$ H₂O (± 248.84 Pa) with $\pm 0.25\%$ accuracy



conceptual design



components



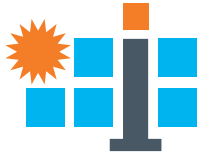
integration



mass production



heliostat field



Wind tunnel experiments – inflow profiles

- Uniform flow

$$U_{\infty} = 10.5 \text{ m/s}, \delta = 0.2 \text{ m}$$

- Turbulent ABL flow

- Mean velocity profile

$$U(z) = \frac{u_{\tau}}{k} \ln \frac{z}{z_0} + d$$

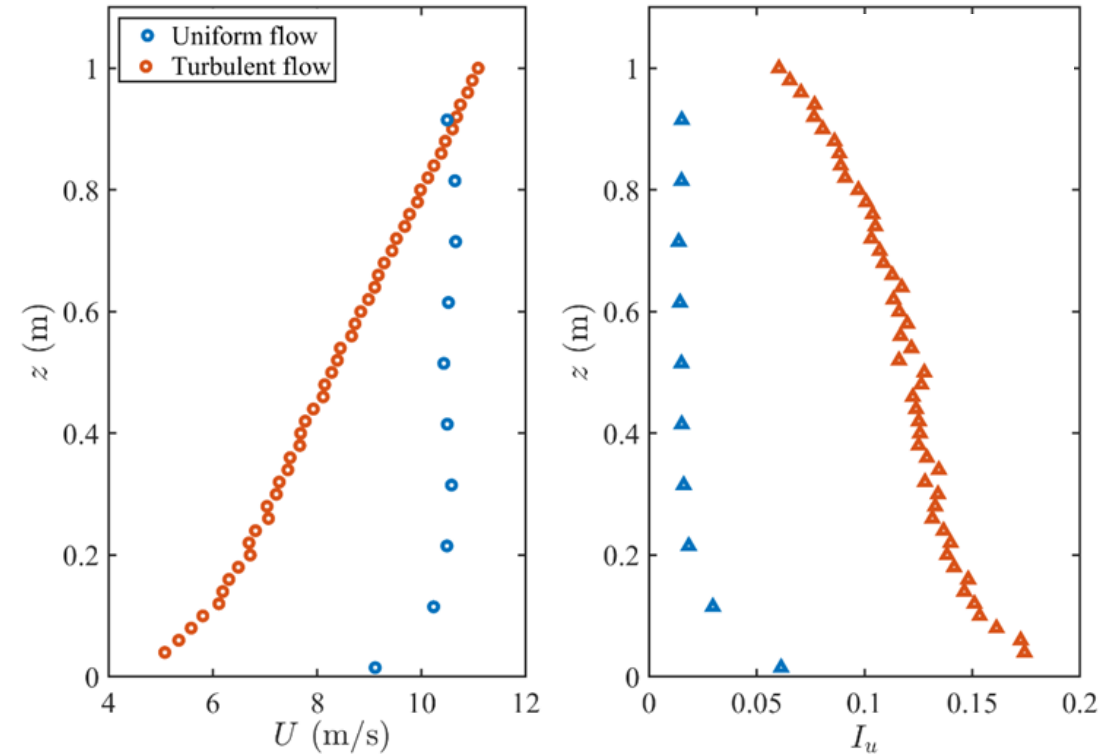
$$u_{\tau} = 0.48 \text{ m/s}, z_0 = 0.01 \text{ m}, d = 4.4$$

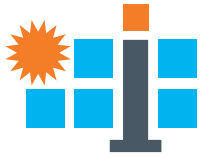
$$U(z) = U_{\infty} \left(\frac{z}{\delta} \right)^{\alpha}$$

$$U_{\infty} = 11.1 \text{ m/s}, \delta = 1.3 \text{ m}, \alpha = 0.35$$

- Turbulence intensity profiles

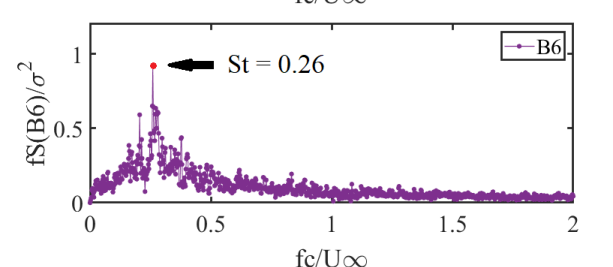
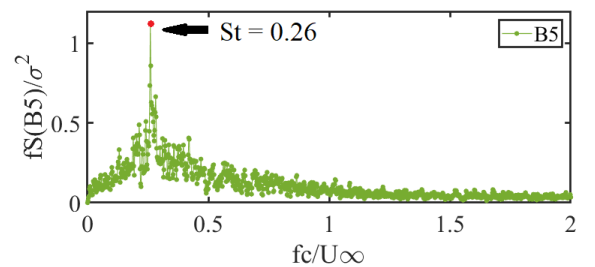
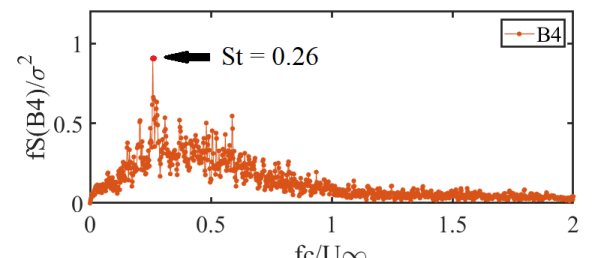
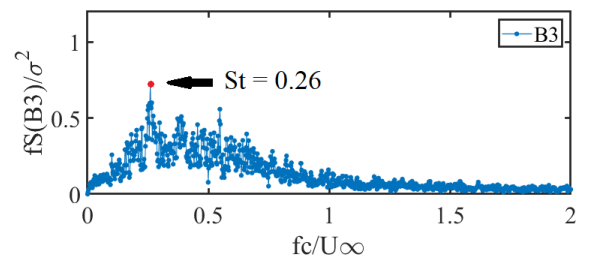
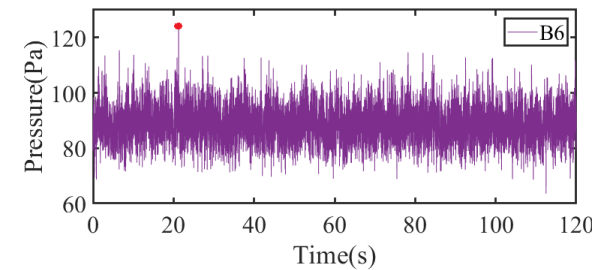
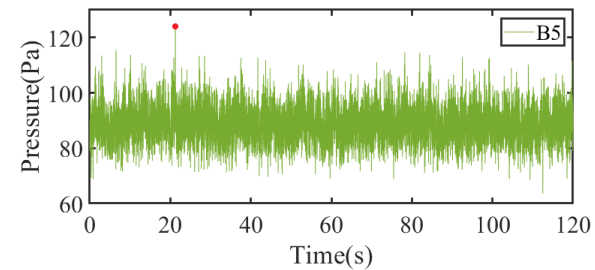
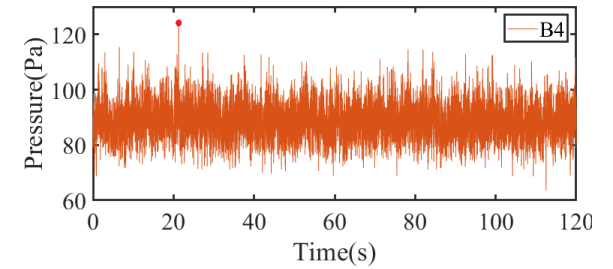
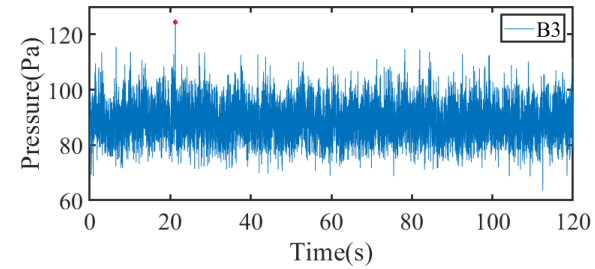
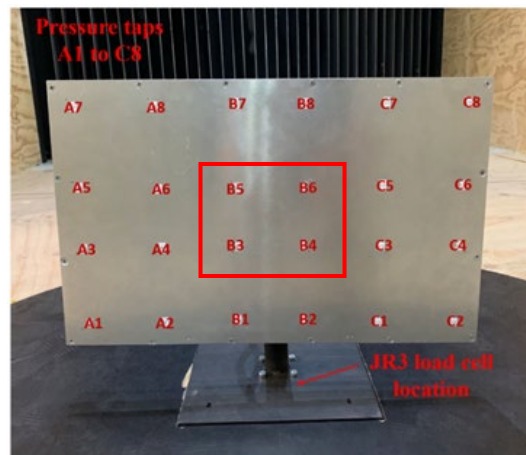
- Open country terrain

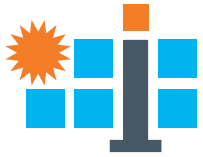




Velocity and spectra time series

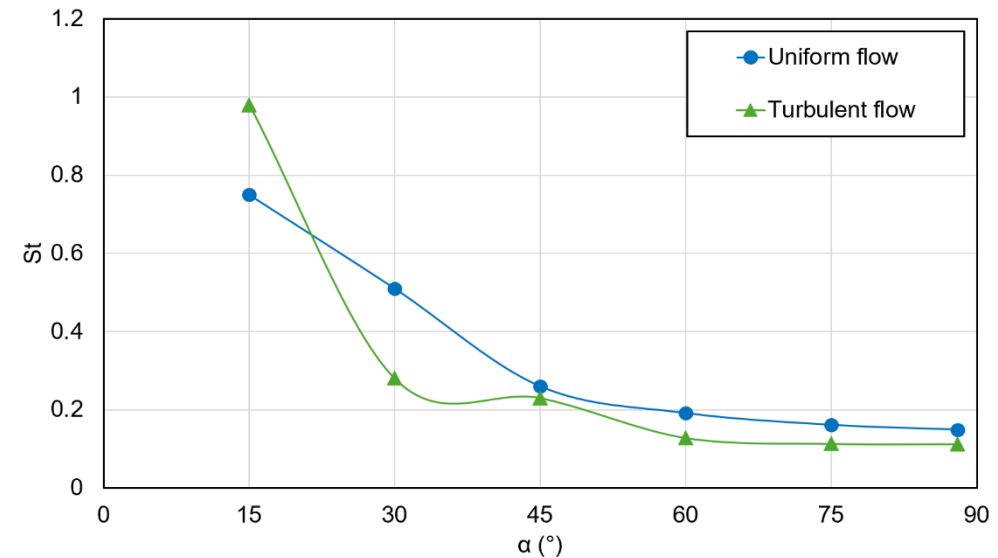
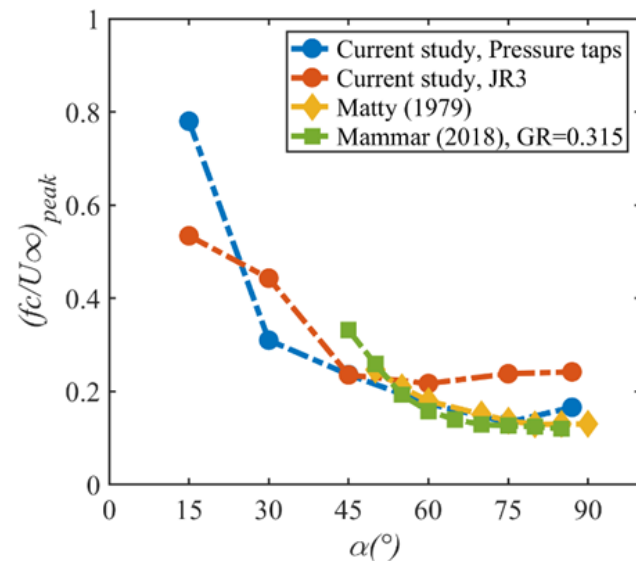
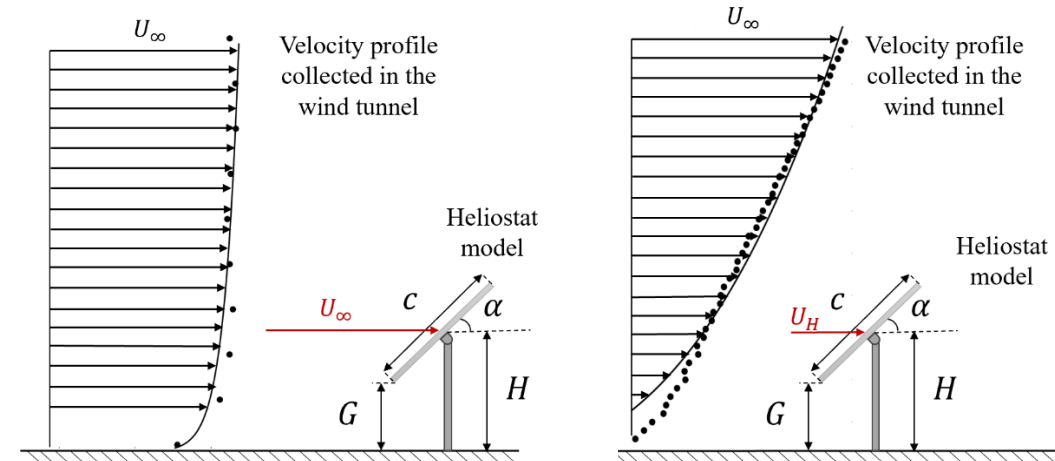
- Case study: $\alpha = 45^\circ$ uniform flow
 - Time series pressure data collected at 1 kHz for 120 seconds
 - PSD (pwelch) of time series data
 - Determine frequency f corresponding to first peak in PSD
 - Determine St as non-dimensional frequency with $c = 0.33$ m and $U_\infty = 11.1$ m/s

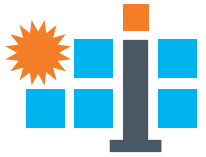




Effect of inflow turbulence

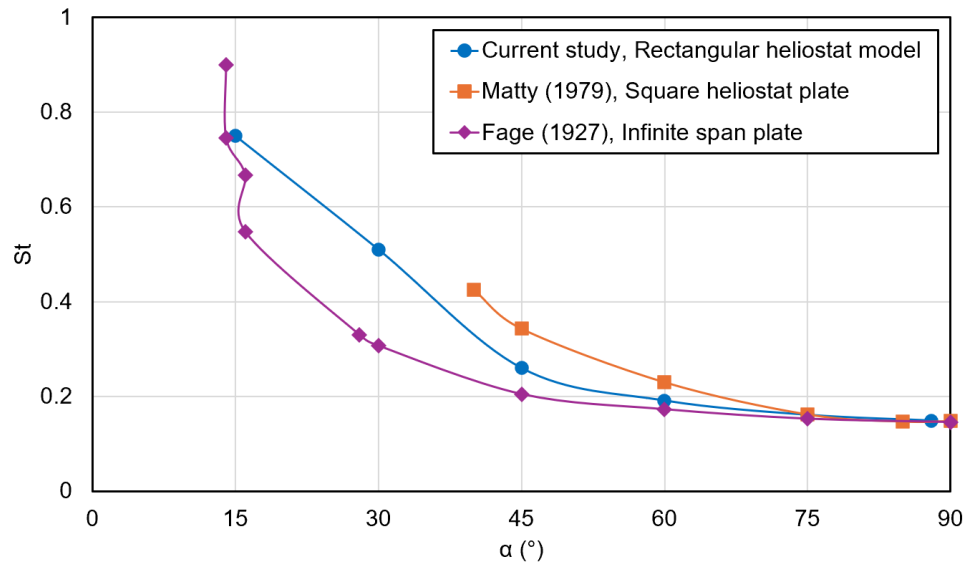
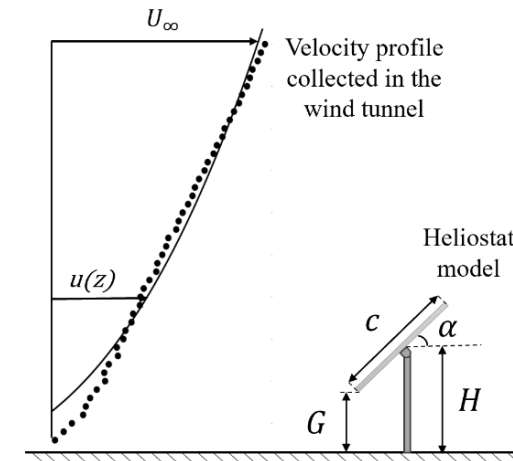
- Impact of inflow turbulence on Strouhal number most significant at $\alpha \leq 30^\circ$
- Strouhal number of flat plate model at $\alpha = 88^\circ$ smaller in turbulent flow than in uniform flow

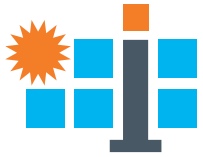




Effect of heliostat elevation angle

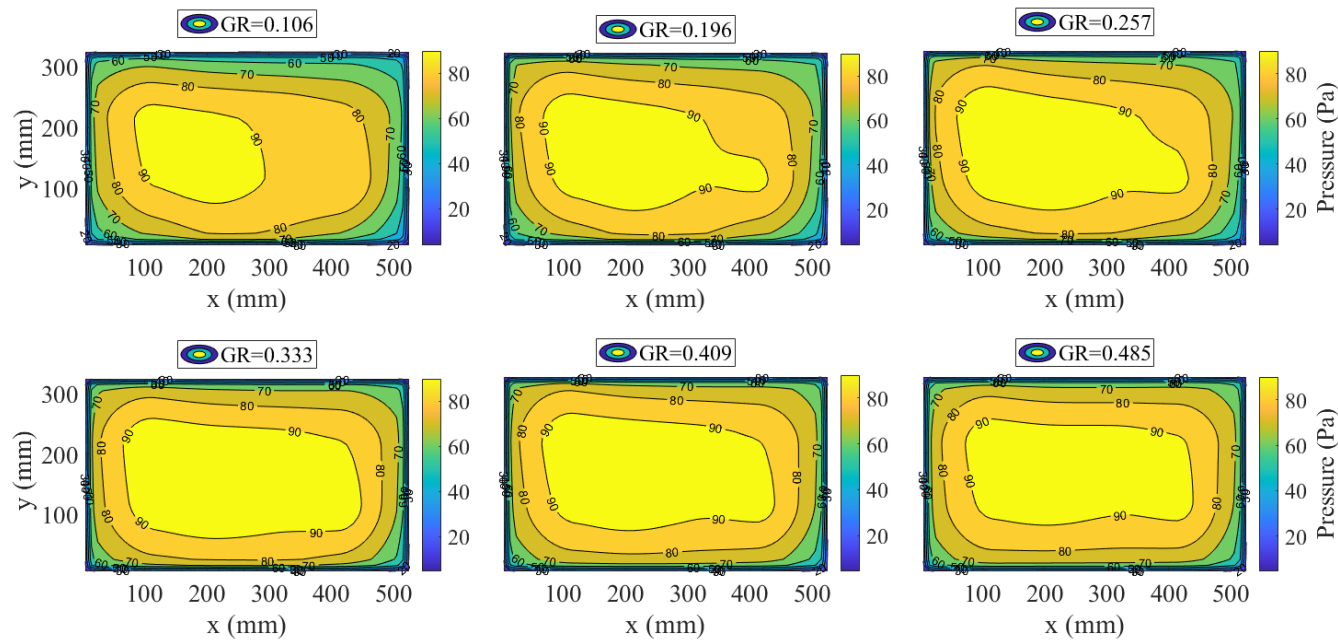
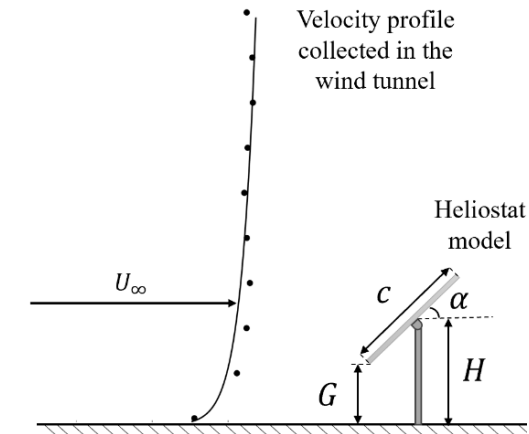
- Strouhal number of a rectangular flat plate is between that of an infinite flat plate and a square flat plate and aspect ratio becomes significant at $\alpha \leq 30^\circ$





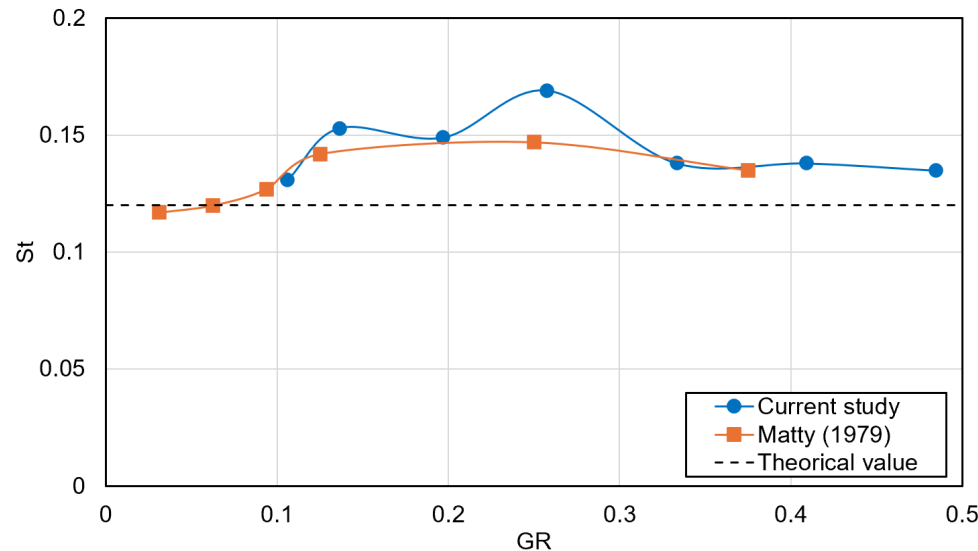
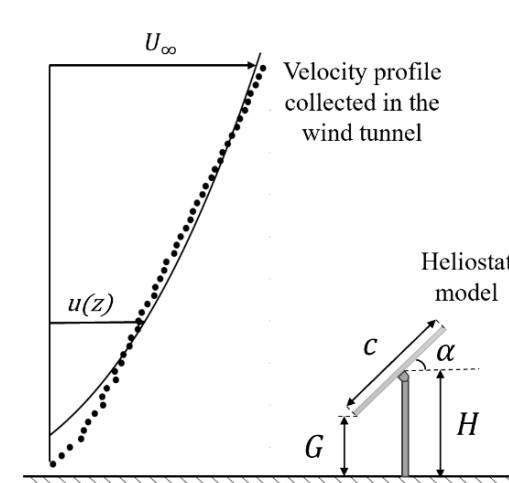
Effect of ground clearance ratio (GR)

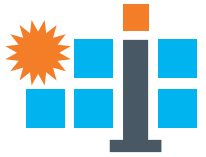
- Asymmetric pressure distribution at $GR \leq 0.257$ in **uniform flow** due to ground effect generating a jet flow with alternate vortex shedding and asymmetric wake



Effect of ground clearance ratio (GR)

- Ground effect causes asymmetric flow and a decrease in Strouhal number at smaller GR
- Flow becomes symmetric at higher GR and Strouhal number approaches a nearly constant value of $St = 0.135$ (0.125 without considering flow effects)

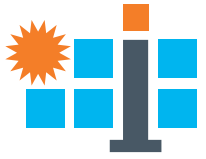




Conclusions and next steps

- Strouhal number of a heliostat model is sensitive to inflow ABL turbulence at elevation angles smaller than 30°
- Strouhal number of a heliostat model is smaller in a turbulent ABL inflow than in a uniform flow for ground clearance ratios of less than 0.4. At larger values of ground clearance ratio, Strouhal number becomes almost constant at 0.15
- As heliostat ground clearance ratio decreases, asymmetric wake is formed in vertical plane and Strouhal number increases while for higher values of ground clearance ratio a symmetric wake is formed and Strouhal number stabilizes at a constant value of 0.135
- Ground clearance effects on Strouhal number at elevation angles of 15° and 30° and the influence of inflow turbulence and azimuth angle on dynamic loads requires further investigation

Acknowledgements



- Heliostat Consortium (HelioCon)

US Department of Energy (DOE) Solar Energy Technologies Office Award DE-EE00038488/38714



- Australian Solar Thermal Research Institute (ASTRI)

Australian Renewable Energy Agency (ARENA) Grant 1-SRI002



Australian Government
Australian Renewable Energy Agency

- University of Adelaide fabrication and instrumentation teams

